

Hydrotreatment of Heavy Oil from Coal Liquefaction on Sulfided Ni–W Catalysts

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Derivados de óleo pesado (temperatura de destilação: 320-340 °C), obtidos a partir do processo de liquefação direta do carvão, usando carvão Shengli foram tratados com hidrogênio usando catalisadores sulfetados Ni–Mo/Al₂O₃, Ni–W/Al₂O₃ e Ni–W/SiO₂ respectivamente. Os catalisadores sulfetados foram caracterizados por BET, XRD, H₂–TPR e NH₃–TPD, respectivamente. As avaliações das propriedades de hidrogenitrogenação (HDN) e hidrodearomatização (HDA) do óleo pesado nos três catalisadores foram realizadas a 400 °C e 5,0 MPa de pressão inicial de H₂. Os catalisadores contendo W mostraram melhores desempenhos do que os catalisadores de Mo para as reações de HDN e HDA. Os catalisadores suportados em Al₂O₃ apresentaram maior atividade catalítica do que aqueles suportados em SiO₂. As atividades dos catalisadores sulfetados foram associadas principalmente à natureza dos sítios ativos, acidez, tamanho do cristalito e da quantidade de espécies redutíveis de enxofre do sulfeto metálico.

Heavy oil (distillation temperature: 320-340 °C) derived from the direct coal liquefaction process using Shengli coal were hydrotreated using sulfided Ni–Mo/Al₂O₃, Ni–W/Al₂O₃, and Ni–W/SiO₂ catalysts respectively. The sulfided catalysts were characterized by BET, XRD, H₂–TPR and NH₃–TPD respectively. The evaluations of the hydrodenitrogenation (HDN) and hydrodearomatization (HDA) properties of heavy oil on the three catalysts were carried out at 400 °C and 5.0 MPa initial H₂ pressure. The W-based catalysts displayed better performances than Mo-based catalysts for the HDN and HDA reactions. Al₂O₃ supported catalysts were found to have higher catalytic activities than on SiO₂ supported ones. The activities of sulfided catalysts were associated mainly with the nature of active sites, acidity, metal sulfide crystallite size and the amount of the reducible sulfur species of metal sulfide.

Keywords: direct coal liquefaction, heavy oil, HDN, HDA

Introduction

With fast increasing demand in liquid transportation fuels and limited petroleum resources, production of transportation fuels from direct coal liquefaction (DCL) technologies has been an important option to lessen the deficiency in petroleum supply.¹

The liquid product obtained from direct coal liquefaction has low hydrogen to carbon ratio and contains a considerable amount of heteroatom compounds that may cause many troubles such as instability of fuel during its transportation or storage.² Nitrogen compounds are certainly an inhibitor in hydrotreatment and cracking processes of these stocks,^{3,4} and lead the catalysts used in the downstream secondary processing (such as fluid catalytic cracking and

hydrocracking) deactivate faster. Such a product must be upgraded to become a feedstock for the existing refineries through extensive removal of heteroatom contained molecules, principally N, S and O in aromatic rings, over sulfided Ni–Mo or Co–Mo catalysts to the acceptable levels in petroleum refining. Moreover the refined products must satisfy the various requirements to be sold in the market, such as cetane index, aromatic content, and sulfur content. Thus, the higher content of nitrogen compounds present in the coal derived heavy oil should be removed prior to further processing.

The aromatic nature of DCL products may be another challenge. Although it can be upgraded to meet all the current specifications for transportation fuels, it may be difficult to keep up with the increasingly stringent specifications in future at an acceptable cost. Novel products upgrading techniques are much needed.¹ Advanced refinery

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technologies, such as hydrodearomatization (HDA), must be implemented in order to fulfill the limits for aromatic contents. Cetane number can also be increased by the HDA process. The hydrogenation of polyaromatics is the main issue in upgrading of coal-derived liquid. Hydrogenation of aromatics is more difficult than hydrodesulfurization (HDS) and hydrodenitrogenation (HDN) due to the types and amount of aromatic species present in the oil as well as the complexity of the reactions.⁵

Many studies have been conducted to investigate the hydrotreatment of coal-derived product on various catalysts.⁶⁻¹² However, few studies focus on the HDA activities on the typical sulfided catalysts based on our knowledge. Industrial HDN and HDS processes have been largely carried out over sulfided Mo-based catalysts promoted with Ni or Co and supported on γ -alumina. However, HDN for high nitrogen content of heavy oil is more difficult and less effective with conventional Ni-Mo/ Al_2O_3 catalyst.¹³ Yoshimura *et al.*¹⁴ found that NiW displays higher HDA activity provided the H_2 pressure is high and the H_2S pressure is moderate to low. Compared to molybdenum-based catalysts, the hydrotreating catalysts based on tungsten are relatively less studied, especially for upgrading of coal-derived liquid.

In this study, the three sulfided catalysts (Ni-Mo/ Al_2O_3 , Ni-W/ Al_2O_3 and Ni-W/ SiO_2) were prepared and characterized by BET (Brunner, Emmet, Teller method), XRD (X-ray diffraction patterns), H_2 -TPR (temperature programmed reduction) and NH_3 -TPD (temperature programmed desorption), respectively. The hydrogenation activity (especially the HDN and HDA activities) of the three sulfided catalysts was evaluated for upgrading of direct coal liquefaction heavy oil.

Experimental

The Shengli coal-derived heavy oil (HO) used was generated from direct liquefaction of Shengli coal in a 0.1 ton/day continuous unit at China Coal Research Institute, Beijing. The direct coal liquefaction reactor was operated at 455 °C and 19 MPa in the presence of Shenhua Fe-based catalyst. The direct coal liquefaction products were separated through high-temperature and low-temperature separators, followed by atmospheric and vacuum distillations. The HO (boiling point: 320-340 °C) used in this study was the narrow fraction of Shengli coal-derived liquid, which are gained by the true boiling point distillation and has high aromatic content (47 wt%) and high nitrogen content (0.4 wt%).

The support material, Al_2O_3 and SiO_2 were provided by Fushun Petrochemical Co. (BET surface area of 185 m^2g^{-1})

and Qindao Ocean Chemical Plant (BET surface area of 408 m^2g^{-1}), respectively.

The loading of Ni-W and Ni-Mo was carried out by incipient wetness impregnation of the support using mixed solutions of ammonium metatungstate and nickel(II) citrate in the case of the Ni-W catalysts, or a mixed solution of ammonium heptamolybdate and nickel(II) citrate for the Ni-Mo catalysts. The impregnated sample was dried and calcined at 500 °C for 3 h. These calcined precursors were then sulfided at 400 °C with a CS_2/H_2 gas (10/90%, 60 mL min^{-1}) for 2 h. The sulfided catalysts were subsequently reduced under H_2 flow for 2 h at 400 °C for evaluating the hydrotreating activities in the batch runs. The sample was then cooled to room temperature and passivated in stream of 1% O_2 for 6 h. The prepared Ni-W or Ni-Mo catalyst contains 5 wt.% Ni and 15 wt.% W or Mo.

BET surface area of the sulfided catalyst was determined by nitrogen adsorption at -196 °C using an ASAP2000 volumetric adsorption analyzer. Total pore volume was calculated from the amount of nitrogen adsorbed at a relative N_2 pressure (P/P_0) of 0.99. The average pore size was assumed to be 4V/BET. All the samples were degassed at 150 °C for 12 h before the measurement.

The acidity of the prepared sulfided catalyst was studied by NH_3 temperature programmed desorption (NH_3 -TPD) in Quantachrome ChemBET-3000 instrument. 0.1 g of sample was loaded into a tubular reactor, and then purged for 2 h with 40 mL min^{-1} helium at 773 K (increased from ambient temperature to 773 K at 10 K min^{-1}), followed by lowering temperature to 353 K. Gaseous ammonia (50 mL min^{-1}) mixed with helium (40 mL min^{-1}) was charged for 30 min at 353 K, and then purged with 40 mL min^{-1} He at 373 K for 1 h. Under the 40 mL min^{-1} of helium, the temperature was raised from 373 to 883 K at 15 K min^{-1} .

Temperature programmed reduction (H_2 -TPR) experiments were carried out in a smaller fixed-bed quartz reactor (2 mm i.d.) coupled with the Hiden QIC-20 mass spectrometer. The transfer line between the fixed-bed reactor and the mass spectrometer was kept at 180 °C. Sulfided samples of 90 mg were heated from room temperature to 800 °C at a rate of 10 °C min^{-1} under a flow of 5% H_2/Ar (50 mL min^{-1}). The evolution of H_2S was analyzed by mass spectrometer.

X-ray diffraction patterns (XRD) of sulfided catalysts were obtained on a Rigaku computer-controlled D/max 2500x using $\text{Cu-K}\alpha$ as the radiation source. During the analysis, catalysts were scanned from 10 to 80° at a speed of 4° min^{-1} .

The hydrogenation experiments of Shengli coal-derived heavy oil were carried out in a 30 mL tubing reactor shaken vertically. 3.0 g of heavy oil was charged into the reactor

together with 0.15 g of sulfided catalyst, which simulates typical online hydrotreating conditions for heavy liquids in direct coal liquefaction with an initial H_2 pressure of 5 MPa and a temperature of 400 °C. After loading the sample, the reactor was sealed and flushed 3 times with hydrogen followed by tuning the system to the desired initial pressure of 5 MPa H_2 . The reactor, agitated vertically at 120 rpm, was submerged into a eutectic salt bath, which had been heated to the desired temperature and maintained for 60 min. After the reaction, the reactor was quenched to ambient temperature in a water bath before the overhead pressure in the reactor was released slowly. The liquid and catalyst in the reactor were removed and separated by centrifugation.

Carbon, nitrogen, and hydrogen analyses were performed using a Elementar Vario EL III. The liquid samples in elemental analysis were sealed in the capsule. Air in the capsule was forced out the capsule via a gas stream of oxygen. The mean blank values of several samples were subtracted for evaluation.

Aromatic distribution analysis was carried out on Shimadzu LC-2000 high performance liquid chromatography with an UV detector ($\lambda = 254$ nm). A Sepax NH_2 (30 cm length, 0.8 cm i.d.) separation column was operated isothermally at 25 °C. Hexane was used as the mobile phase with a flow rate of 1.2 mL min^{-1} . The identification of aromatic components (biaromatic and triaromatic) was carried out by the retention time of selected representative components of the mono, di and triaromatic groups (toluene, naphthalene, anthracene and phenanthrene).

Results and Discussion

The BET surface area, pore volume and pore size distribution of three sulfided catalysts are given in Table 1. It shows that the drastic reduction of the specific surface area was observed. Compared to the specific surface areas of supports, the specific surface areas of sulfided Ni–Mo/ Al_2O_3 , Ni–W/ Al_2O_3 and Ni–W/ SiO_2 catalysts decreased by about 33%, 21% and 40% respectively. This decrease in specific surface area could be attributed to the lower amount of support in the catalyst (only about 70% of the catalyst is support and contributes for the surface area) and the presence of particles of Ni–W(Mo)–S and WS_2 or MoS_2

partially blocking the mesopores. Compared to Ni–W/ Al_2O_3 , Ni–Mo/ Al_2O_3 shows lower surface area, pore volume and mean pore radius, revealing a poor dispersion of the active phases or a higher blockage of mesopores. For Ni–W based catalyst, Al_2O_3 supported catalyst displayed higher pore volume and mean pore radius compared to SiO_2 supported one. The observed textural differences can be attributed to the differences of the active phase and the type of support.

The N_2 adsorption-desorption isotherms of sulfided catalysts are shown in Figure 1. All the sulfided catalysts exhibited the typical type IV isotherms according to the Brunauer-Deming-Deming-Teller (BDDT) classification, which exhibited the condensation and evaporation step characteristic of common mesoporous materials. The pore diameter distribution curves of the samples are shown in Figure 2. Compared with the Ni–Mo/ Al_2O_3 catalyst it clearly shows that Ni–W/ Al_2O_3 exhibited a bimodal distribution of pore size, which may indicate that the addition of W mainly blocks the mesopores. For Ni–W/ SiO_2 sample, the pore diameter ranges were narrow (between 3 nm and 15 nm).

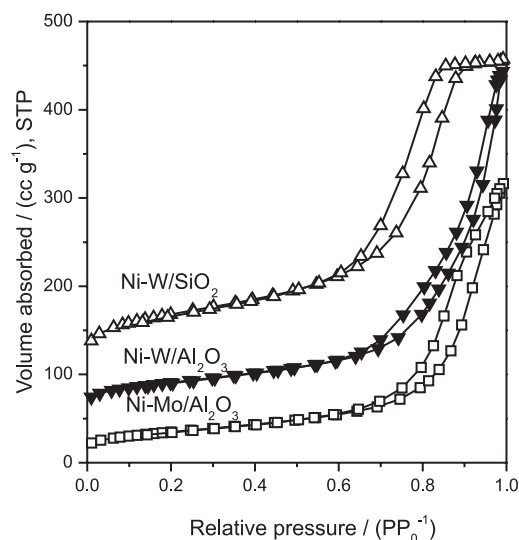


Figure 1. The nitrogen-adsorption/desorption isotherms of sulfided catalysts.

Figure 3 shows the X-ray diffraction patterns of the three sulfided catalysts. It can be seen that two Al_2O_3 -based catalysts display only broad peaks of the alumina support. No characteristic peaks of NiS_2 , MoS_2/WS_2 phases, NiO

Table 1. Textural property of sulfided catalysts

Catalyst	Surface area / ($m^2 g^{-1}$)	Pore volume / ($cm^3 g^{-1}$)	Mean pore radius / nm
Ni–Mo/ Al_2O_3	124	0.489	15.8
Ni–W/ Al_2O_3	147	0.609	16.6
Ni–W/ SiO_2	246	0.553	9.0

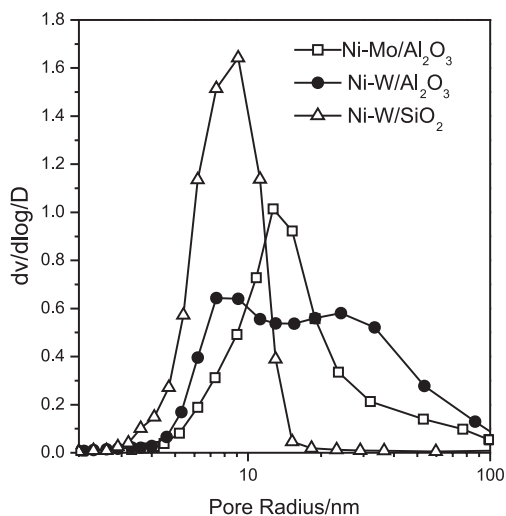


Figure 2. The pore size distributions of sulfided catalysts.

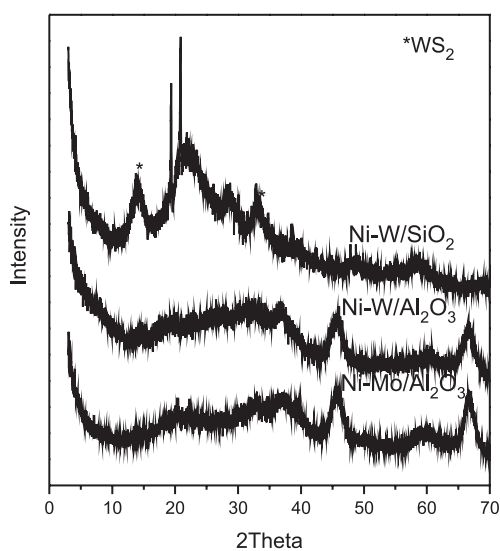


Figure 3. X-ray diffraction patterns of sulfided catalysts.

and MoO_3/WO_3 , metallic nickel /tungsten phase can be observed. This indicates that Ni and Mo/W species were considered uniformly distributed on the surface of the Al_2O_3 support under preparation conditions. Also, the absence of diffraction lines of nickel or tungsten sulfide could indicate that these phases have a very small particle size or that they are inserted into the structure of WS_2 or MoS_2 , forming a well dispersed Ni-W(Mo)-S nanoclusters.¹⁵ But for Ni-W/ SiO_2 catalyst, the WS_2 phases can be confirmed. This result indicates that the SiO_2 support led to larger size of W cluster size, which may result from the temperature of calcinations for SiO_2 is too high.

The TPD of NH_3 is a useful tool to measure the acidity and its distribution of the catalyst. The NH_3 -TPD profiles for the three sulfided catalysts are completely different as shown in Figure 4. To compare the acidity distribution

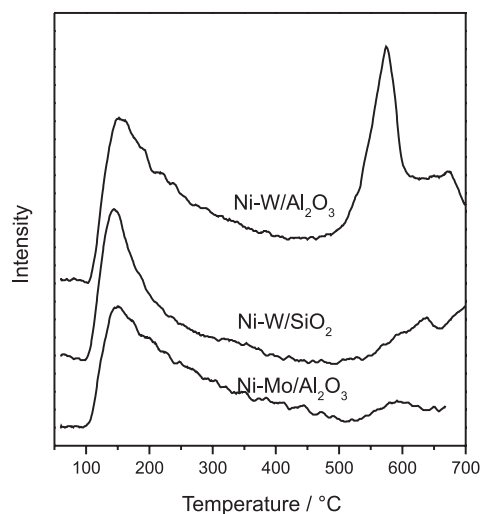


Figure 4. The NH_3 -TPD profiles of sulfided catalysts.

among the catalysts, the weak, medium, and strong acidities were assigned to the peak areas of NH_3 -TPD curves below 623 K, at 623-773 K, and above 773 K, respectively.¹⁶ The sulfided Ni-Mo/ Al_2O_3 catalyst showed one broad peak at the temperature range of 100-500 °C, which is attributed to the weak acid sites (74%) and medium acid sites (14%). The sulfided Ni-W/ SiO_2 catalyst showed an increase both in the strong acid sites by 10%, compared to the sulfided Ni-Mo/ Al_2O_3 catalyst. The sulfided Ni-W/ Al_2O_3 catalyst showed significant increase of amount of the strong acid sites by 23% compared to the sulfided Ni-W/ SiO_2 catalyst. The NH_3 -TPD results confirm the significant difference of acid sites on the sulfided catalyst surface. Several works proved that strong acid sites are closely related to hydrogenation activity. The strong acid site is probably due to the formation of another active phase on the catalyst, which reduces the interaction between NiMoS and Al_2O_3 .¹⁷ Many literatures^{18,19} proved that strong acid sites on the catalyst surface are responsible for the enhancement of HDN activity of the catalysts. The higher acidity led to higher conversion.

The TPR was performed for three sulfided catalysts to study the extent of a reaction of hydrogen with the sulfide species present on the sulfided catalyst surface. Figure 5 shows the evolution of H_2S during H_2 -TPR processes. The evolution peak of H_2S is probably due to the reaction of NiS_2 , MoS_2 or WS_2 with H_2 .¹⁸ It can be seen that the three samples showed quite different behaviors in H_2S evolution profiles. For the sulfided Ni-Mo/ Al_2O_3 catalyst there were mainly two H_2S evolution peaks, which were in the temperature ranges of 100-250 °C and 350-700 °C, respectively. The sulfided Ni-W/ SiO_2 catalyst also had two H_2S evolution peaks during H_2 -TPR process, but the temperature ranges shifted to 150-400 and 500-800 °C compared to the sulfided Ni-Mo/ Al_2O_3 catalyst, respectively. The sulfided Ni-W/

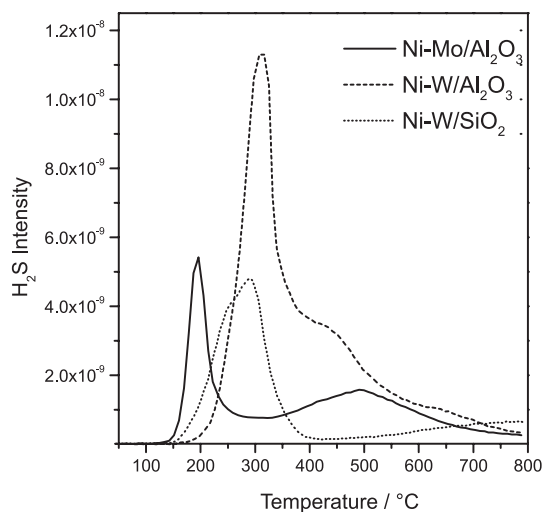


Figure 5. H₂-TPR profiles for sulfided catalysts.

Al₂O₃ catalyst showed significant increase of amount of H₂S evolution between 200 to 800 °C, compared to the sulfided Ni–Mo/Al₂O₃ and Ni–W/SiO₂. The H₂S evolution peak for Ni–W/Al₂O₃ was larger than those of Ni–Mo/Al₂O₃ and Ni–W/SiO₂, indicating much reduction of WS₂ and NiS₂. Nag *et al.*²⁰ suggested that surface reaction between surface anion and H₂ forms surface anion vacancy, which has been frequently suggested as catalytic active sites for HDS and other hydroprocessing reactions.

The HO used in this experiment, which is characterized by high aromatic content and high nitrogen content, is a typical coal-derived liquid feed stock for hydrotreatment. The color of HO as received is black. After hydrogenation, the color of HO turned from black to yellow. During prolonged storage of hydrogenated HO it was found that the color of HO after hydrogenation slowly turned from yellow to black, especially in air, which agrees with Begon's finding.²¹ But HO hydrogenated on Ni–W/Al₂O₃ catalyst is more stable than that of others (as shown in Figure 6), which



Figure 6. Photos of heavy oil (HO) and its hydrogenation products on sulfided catalysts.

indicates that the catalyst structures affect the stability of heavy oil after hydrotreatment. Further work on the storage stability of coal-derived liquid has been carrying out in our laboratory.

Figure 7 shows the HDN activities of the three sulfided catalysts. It shows that HDN conversion of sulfided Ni–Mo/Al₂O₃ catalyst was 27%, which indicates that the nitrogen of HO is difficult to remove. Compared with sulfided Ni–Mo/Al₂O₃ catalyst, sulfided Ni–W/Al₂O₃ catalyst and Ni–W/SiO₂ exhibited much higher HDN activity. The HDN activities of sulfided Ni–W/Al₂O₃ and Ni–W/SiO₂ catalysts increased by 33% and 10%, respectively compared to that of Ni–Mo/Al₂O₃. These results indicate that W-based sulfided catalysts have higher HDN activity than that of Mo-based sulfide catalysts towards coal-derived heavy oil hydrogenation and the type of support also significantly affect of HDN activity. Higher HDN activities were found on the Al₂O₃ than those on SiO₂ supported catalysts.

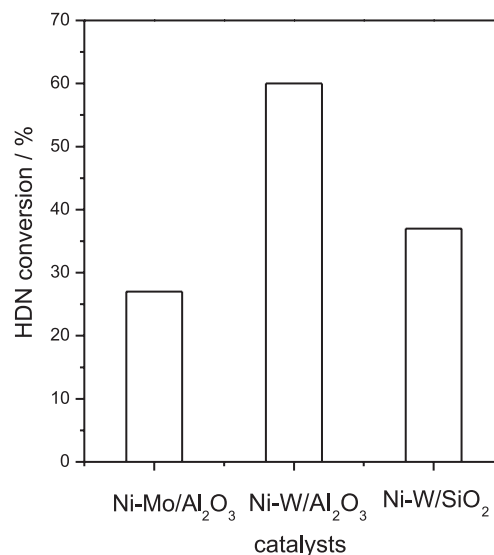


Figure 7. HDN conversion of HO over sulfided catalysts.

Another aim of HO hydrogenation is to increase the H/C atomic ratio of product. Figure 8 shows the H/C atomic ratio of HO before and after hydrogenation on three sulfide catalysts. It can be seen that the change of H/C atomic ratio after hydrogenation on three sulfide catalysts was significantly different. Sulfided Ni–Mo/Al₂O₃ caused only small increment of the H/C ratio. As compared to sulfided Ni–Mo/Al₂O₃ catalyst, the H/C ratio was significantly increased for Ni–W/Al₂O₃ catalyst and Ni–W/SiO₂, and the highest H/C ratio was obtained for Ni–W/Al₂O₃. The result of the change of H/C atomic ratio indicates that the hydrogenation activities follow the order: Ni–W/Al₂O₃ > Ni–W/SiO₂ > Ni–Mo/Al₂O₃.

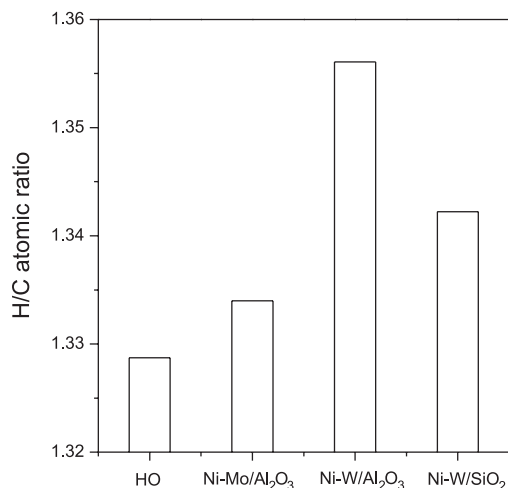


Figure 8. H/C atomic ratio of HO and its hydrogenation products over sulfided supported catalysts.

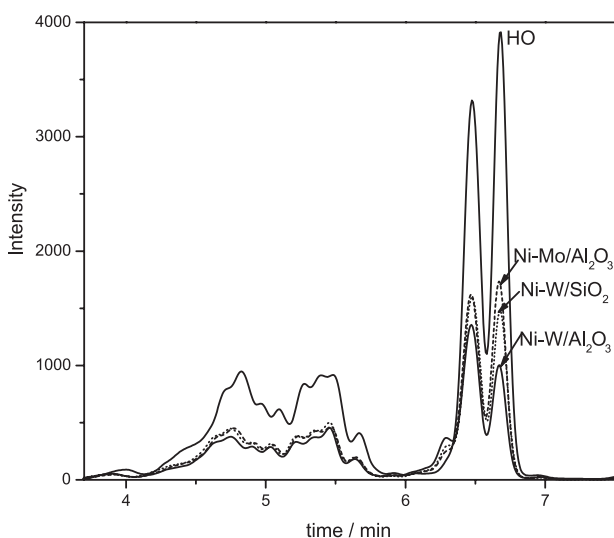


Figure 9. Aromatic distribution of HO and its hydrogenation products on different catalysts.

Figure 9 shows the aromatic distribution of the feedstock (HO) and its hydrogenation products on the three sulfided catalysts. It shows that aromatic of HO mainly contained diaromatics (naphthalene and its derived) and triaromatics (anthracene and phenanthrene). After hydrogenation, the amounts of aromatic significantly decreased on all the catalysts. Table 2 shows the HDA activities of three sulfided catalysts. It shows that the HDA activities of sulfided Ni-Mo/Al₂O₃, Ni-W/Al₂O₃ and Ni-W/SiO₂ catalysts were 50%,

58% and 50%, respectively. For sulfided Ni-Mo/Al₂O₃, the HDA activities of diaromatics and triaromatics were almost the same. But for sulfided Ni-W/Al₂O₃ and Ni-W/SiO₂ catalysts the HDA activities of triaromatics were higher than that of diaromatics by 5%. This result indicates that active phase-W can significantly increase HDA activities of triaromatics compared with that of diaromatics. In order to gain some insights into the reactivity of HO, the HDA activity of triaromatic (anthracene and phenanthrene) were calculated in Table 2. It can be seen that hydrogenation of HO on the sulfided Ni-Mo/Al₂O₃ resulted in a 49% and 55% decrease of anthracene and phenanthrene, respectively. In the presence of Ni-W/SiO₂ the conversions of anthracene and phenanthrene were 49% and 61%, respectively. However, in the presence of Ni-W/Al₂O₃ the conversions of anthracene and phenanthrene were 55% and 74%, respectively. These results indicate that active phase-W can significantly increase the hydrogenation of phenanthrene for about 19% compare to that of active phase-Mo. Also Absi-Halabi *et al.*²² found that asphaltene conversion for Ni-W/Al₂O₃ was higher than that of Ni-Mo/Al₂O₃ during hydrotreating of petroleum residues. However, it should be noted that the presence of polyaromatic compounds could lead to coke formation, which can lead to catalyst deactivation. Further testing should be required to explore the deactivation of W-based catalysts.

From the above characterizations of three sulfided catalysts it can be observed that Ni-W/Al₂O₃ had higher pore volume and larger pore size, which indicates that Ni-W/Al₂O₃ may be more favorable for the diffusions of reactants and products compared with Ni-Mo/Al₂O₃ and Ni-W/SiO₂, especially for the diffusion of coal-derived heavy oil. Since HDN and HDA activities are dependent not only on the physical surface area but also on the other surface physicochemical properties of the catalyst. NH₃-TPD and H₂-TPR showed that the acidities and the amount of the reducible sulfur species of metal sulfide followed the same order: Ni-W/Al₂O₃ > Ni-W/SiO₂ > Ni-Mo/Al₂O₃. The activity evaluation results showed that the stability of heavy oil after hydrotreatment, HDN and HDA activities also followed the same order: Ni-W/Al₂O₃ > Ni-W/SiO₂ > Ni-Mo/Al₂O₃. The relative hydrogenation activity of Ni-W was higher than that of Ni-Mo. Such difference in hydrogenation may be attributed to the difference in the

Table 2. HDA activities of the three sulfided catalysts

	HDA / (%)	HDA(bi) / (%)	HDA(tri) / (%)	HDA (anthracene) / (%)	HDA (phenanthrene) / (%)
NiMo/Al ₂ O ₃	50	51	50	49	55
NiW/Al ₂ O ₃	58	56	61	55	74
NiW/SiO ₂	50	50	55	49	61

nature of active sites. Laetitia Oliviero proposed that the activity pattern of NiMo catalysts in HDS and in HDN results from the synergy between nickel and molybdenum in contact with each other on an adequate support, after sulfidation.²³ Then, the synergy effect between Ni and W is stronger than that of Ni and Mo. All the results above indicate that the higher hydrogenation activity of sulfided catalysts for coal-derived heavy oil upgrading is associated not only with the nature of active sites and larger pore size but also with the strong acidic sites, metal sulfide crystallite size and the formation of S anion vacancies. The orders of HDN and HDA activities are correlated to the orders of the strong acid sites and the amount of the reducible sulfur species of metal sulfide for three sulfided catalysts. This result indicates that the activities of sulfided catalysts are associated mainly with the nature of active sites, acidity and the amount of the reducible sulfur species of metal sulfide. The findings of the present study provide useful information for the development of better catalysts for the efficient HDN and HDA of coal-derived heavy oil.

Conclusions

HO derived from the direct coal liquefaction process of Shengli coal was hydrotreated in the presence of Mo-based or W-based sulfided catalyst at 400 °C. The results suggest that the active phase and type of support significantly affect the HDN and HDA activities. The W-based sulfided catalysts had high hydrogenating activity. Higher catalytic activities were found on the Al₂O₃ than on SiO₂ supported catalysts. The HDN and HDA activities of sulfided Ni–W/Al₂O₃ were about 60% and 58% at 400 °C and initial 5 MPa H₂ respectively. Ni–W/Al₂O₃ had better hydrogenation activity towards triaromatics, especially for the hydrogenation of phenanthrene (the activity increases about 19% compared to that of Ni–Mo/Al₂O₃). The activities of sulfided catalysts are associated mainly with the nature of active sites, acidity, metal sulfide crystallite size and the amount of the reducible sulfur species of metal sulfide.

Acknowledgments

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References

1. Liu, Z.; Shi, S.; Li, Y.; *Chem. Eng. Sci.* **2010**, *65*, 12.
2. Perot, G.; *Catal. Today* **1991**, *10*, 447.
3. Dorbon, M.; Ignatiadis, I.; Schmitter, J. M.; Arpino, P.; Guichon, G.; Toulhoat, H.; Huc, A.; *Fuel* **1984**, *73*, 565.
4. Fathoni, A. Z.; Batts, B. D.; *Energy Fuels* **1992**, *6*, 681.
5. Stanislaus, A.; Cooper, B. H.; *Catal. Rev. - Sci. Eng.* **1994**, *36*, 75.
6. Liaw, S.; Keogh, R.; Thomas, G.; Davis, B.; *Energy Fuels* **1994**, *8*, 581.
7. Sumbogo Murtia, S. D.; Choia, K.; Sakanishib, K.; Okumac, O.; Koraiia, Y.; Mochida, I.; *Fuel* **2005**, *84*, 135.
8. Sarbak, Z.; Lewandowski, M.; *Appl. Catal., A* **2001**, *208*, 317.
9. Raje, A.; Liaw, S.; Chary, K.; Davis, B.; *Appl. Catal., A* **1995**, *123*, 229.
10. Liaw, S.; Lin, R.; Raje, A.; Davis, B.; *Appl. Catal., A* **1997**, *151*, 423.
11. Raje, A.; Liaw, S.; Srinivasan, R.; Davis, B.; *Appl. Catal., A* **1997**, *150*, 297.
12. Liaw, S.; Raje, A.; Thomas, G.; Davis, B.; *Appl. Catal., A* **1997**, *150*, 343.
13. Ferdous, D.; Dalai, A. K.; Adjaye, J.; *Ind. Eng. Chem. Res.* **2006**, *45*, 544.
14. Yasuda, H.; Higo, M.; Yoshitomi, S.; Sato, T.; Imamura, M.; Matsubayashi, H.; Shimada, H.; Nishijima, A.; Yoshimura, Y.; *Catal. Today* **1997**, *39*, 77.
15. Rodriguez-Castellón, E.; Jiménez-López, A.; Eliche-Quesada, D.; *Fuel* **2008**, *87*, 1195.
16. Ding, L.; Zheng, Y.; Zhang, Z.; Ring, Z.; Chen, J.; *J. Catal.* **2006**, *241*, 435.
17. van Veen, R. A. J.; Colijn, M. A.; Hendriks, P. A. J. M.; van Welsenes, A. J.; *Fuel Process. Technol.* **1993**, *35*, 137.
18. Ferdous, D.; Dalai, A. K.; Adjaye, J.; *Appl. Catal., A* **2004**, *260*, 153.
19. Ding, L.; Zheng, Y.; Zhang, Z.; Ring, Z.; Chen, J.; *Appl. Catal., A* **2007**, *319*, 25.
20. Nag, N. K.; Fraenkel, D.; Moulijn, J. A.; Gates, B. C.; *J. Catal.* **1980**, *66*, 162.
21. Begon, V.; Suelves, I.; Herod, A. A.; Dugwell, D. R.; Kandiyoti, R.; *Fuel* **2000**, *79*, 1423.
22. Absi-Halabi, M.; Stanislaus, A.; Al-Dolama, K.; *Fuel* **1998**, *77*, 787.
23. Rocha, A. S.; Faro Jr., A. C.; Oliviero, L.; Gestel, J. V.; Maugé, F.; *J. Catal.* **2007**, *252*, 321.

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