

Article

Indirect Determination of Ethanol in Drinks Using a Capacitance Flow-through Detector

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Foi desenvolvido um método de análise para a determinação de vapor de água, baseado num sensor capacitométrico. Este detector consiste de dois tubos concêntricos de aço inoxidável e fica localizado no tubo de amostragem da válvula introdutora de amostra do sistema de fluxo. O logaritmo da capacitância dos vapores de amostra (sinal analítico) apresenta uma boa correlação linear com a concentração de vapor de água numa faixa de 1705 até 2197 Pa. Cerca de 55 amostras podem ser analisadas por hora. Este sistema de fluxo foi aplicado à determinação indireta da concentração de etanol em bebidas alcoólicas, em função da concentração do vapor de água presente no frasco contendo o líquido em análise. Não é necessário nenhum pré-tratamento da amostra. Corantes presentes na bebida não interferem nos resultados.

A flow procedure based on a metallic capacitance flow-through detector is described for the analysis of water vapour. The capacitance detector consists of two stainless steel tubes and is located in the loop of a sampling valve. The logarithm of the capacitance signal correlates linearly with the concentrations of water vapour in the 1705 to 2197 Pa range. A sampling frequency of about 55 h⁻¹ can be achieved. The flow system was applied to the indirect determination of the ethanol concentration in drinks based on the analysis of water vapour content above the liquid sample, without any pre-treatment of the sample. The colour of the drinks has no effect on the measurements.

Keywords: *capacitance, water vapour, ethanol, drinks, flow analysis*

Introduction

The capacity is defined as the charge that the capacitor can store per unit of potential difference between the plates. The capacity of a condenser is increased by interposing a dielectric material between the plates. In tensammetry the capacitance of the electrical double layer of an electrode is measured. The capacitance value is strongly influenced by the presence of absorbing species¹. Although tensammetry is possible at all kinds of electrode surfaces, mercury is the most widely used electrode material¹. Detectors with mercury electrodes (dropping mercury^{2,3}, hanging or static modes⁴ and mercury-coated¹ are mainly used for the determination of substances in solutions. Other electrode materials, based on the capacitance principle, have also been developed. A tantalum capacitance sensor is used for the detection of proteins by immunochemical binding reactions⁵. Berggren and Johansson immobilised monoclonal antibodies on gold substrates⁶. The antibody layers and their interactions with antigens in solution were investigated with capacitance measurements and with cyclic vol-

tammetry. The capacitance change versus the logarithm of antigen concentration is linear over three decades⁶. A gas-sensitive semiconductor based on a palladium MOS field-effect capacitor for the determination of ammonia in air and aqueous solutions has also been described⁷. The main problem in preparing a stationary working electrode for tensammetric measurements is the formation of a homogeneous and well-defined surface¹.

Double layers are not a special feature of the electrode-electrolyte interfaces; they are a general consequence of the junction of two phases at a boundary⁸. Owing to its high dielectric constant (78.5 at 25 °C) water is the primary species which can be measured by changes of the capacitance⁹. Many industrial processes, such as drying, baking, kilning, etc., involve the modification of a material water content. The measurement of humidity should rate equally in importance with the measurement of temperature in industry¹⁰. The aim of this work was to evaluate a proposed metallic capacitance detector for quantitative analysis of gases and to develop a fast procedure for measurement of water vapour in a flow system. The proposed method is

Table 1. Capacitance signal and vapour pressure of tested substances in flow analysis*.

Tested substance	Signal / nF	Gas or vapour pressure at 25 °C / kPa ¹⁴
Room air	0.002	ca 101.3**
Carbon dioxide	0.002	ca 101.3**
Water	1.473	3.2
Methanol	0.001	16.7
Ethanol	0	8.0
Benzene	0.265	1.6 ^{24.5***}
Toluene	0.819	0.8 ^{35.4***}
Chloroform	0.608	26.0
Acetone	0.017	24.2 ²⁰
Acetic Acid	0.001	2.0

* Liquid samples maintained at a temperature of 20.0 °C. Sampling and interval time = 50 and 15 s. Flow rates of sample and air carrier = 21 and 330 mL min⁻¹. The detector operated at room temperature (about 22 °C).

** Carbon dioxide gas, obtained from a cylinder, and air directly introduced into the analytical system at a pressure of about 1 atm.

*** Tomáš Boublík; Vojtech Fried; Eduard Hála; Physical sciences data 17: *The vapour pressure of pure substances, Selected values of the temperature dependence of the vapour pressures of some pure substances in the normal and low pressure region*, 2nd., Elsevier, 1984.

responses. Therefore water vapour was chosen to study the response characteristics of the detector. A typical recorded curve for water vapour is shown in Fig. 2. The signal peak is asymmetric. The detector begins to respond to water vapour about 6 s after the sample vapour passes through the detector. When the sampling valve is switched to the rinsing position only the filtered dried air carrier is passing through the detector and the signal rapidly returns to baseline. The experiments were carried out with a stop-watch, and it can be expected that the application of solenoid valve control sampling may improve the repeatability of the measurements. It is necessary to use a sampling time longer than 6 s in order to obtain an observed signal. The time of 10 s is enough for returning the signal to the baseline, allowing the introduction of the next sample.

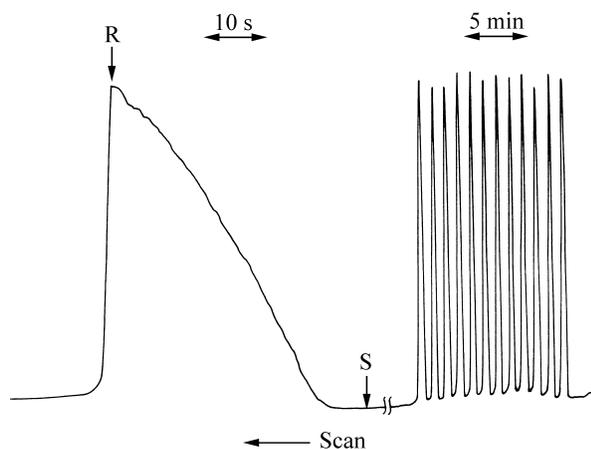


Figure 2. A recorded curve for the response of water vapour in the flow system. Water was maintained at 20.0 °C. Sampling 40 s and interval 20 s. S was the time point of sampling and R was that of rinsing.

The effect of sampling time up to 90 s was evaluated and results are shown in Fig. 3. After a delay of several seconds, the signal rapidly increases as the time of sample vapour passing through the detector increases. Since the analytical frequency depends on the sampling time, a compromise between sample throughput and sensitivity was made, and a sampling time of 40-50 s and an interval time of 15 s were chosen. Thus, the analytical frequency is at least 55 samples h⁻¹.

Another factor influencing the analytical signal is the flow rate of sample vapour. Below a flow rate of 20 mL min⁻¹, the signal increases with increasing flow rate of

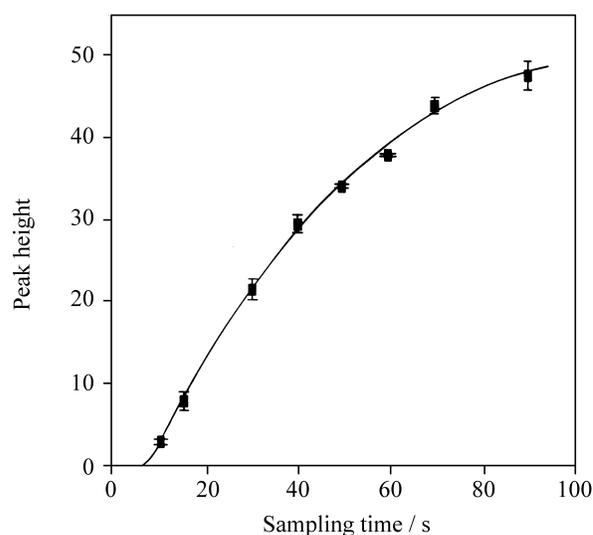


Figure 3. Effect of sampling time on the signal. Water was maintained at 20.0 °C. Interval time was 15 s. Average values corresponding to four determinations at the same sampling time.

water vapour; after 20 mL min⁻¹ the signal remains constant. This fact may be understood in terms of the saturation of the electrode with the vapour. The sample flow rate was selected at 21 mL min⁻¹.

2. Relationship of the capacitance signal and the concentration of water vapour

The relationship between the capacitance signal and the water vapour concentration was tested. The capacitance signal is not linear with respect to the concentration of water vapour. The logarithm of the net capacitance signal, measured as peak height, however, linearly correlates to the concentrations of water vapour in the range of 1705 to 2197 Pa. This correlation is used as the calibration curve. The features of the determinations of water vapour with different sampling time are summarised in Table 2.

3. Selectivity

When the capacitance flow-through detector was used for the measurement of gases or vapours in the flow system, it shows some selectivity as it responds to only some organic vapours. The proposed method is suitable for well-defined samples, for example, indirect determination of ethanol in drinks as the water vapour pressure depends on the ethanol concentration of the solution.

4. Analytical application: Indirect determination of ethanol in drinks

Since ethanol has hardly response in the capacitance detector under the experimental conditions (see Table 1), the relationship between capacitance signal and ethanol content in water was studied and is shown in Fig. 4. The recorded signal is dependent on the concentration of ethanol in the sample. The logarithm of the analytical signal is inversely proportional to the ethanol content of the solution. The features of the determination of ethanol with different sampling times are also given in Table 2. The logarithm of the capacitance signal measured as peak

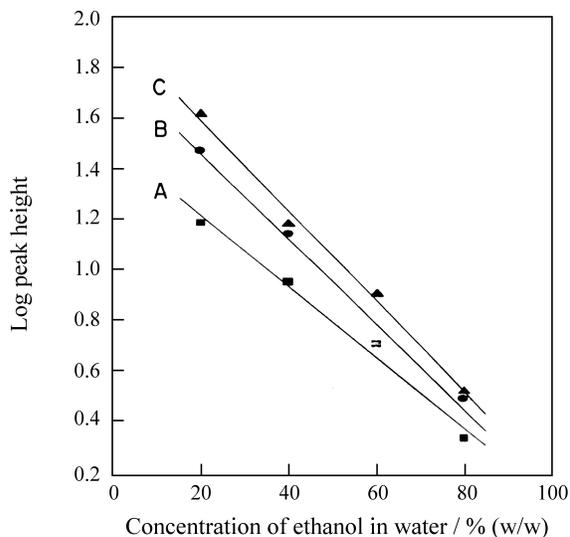


Figure 4. Calibration curves of logarithm of the capacitance signal and concentration of ethanol in water. Curves A, B and C indicate sampling times of 20, 40 and 60 s, respectively.

height linearly correlates to the concentrations of ethanol in water over a limited working range.

The proposed method was applied to determine indirectly the ethanol content in drinks. The vapours of drink samples are analysed directly without any pre-treatment. The results obtained in this work are compared with those using the density method by another laboratory and given in Table 3. The colours of the drinks have no effect on the measurements.

Conclusions

The metallic electrode proposed in this work can be used as a capacitance detector for the measurement of water vapour and, as a consequence, of substances that can change the vapour pressure of the water. It does not present the problem of surface renewal and was easy to operate. It provides a stable baseline and can be made as a portable instrument. The proposed method was employed to indi-

Table 2. Relationship between logarithm of capacitance signal and concentrations of water vapour and of ethanol.

Sampling time / s	Equation*	Correlation coefficient	Detection limit / Pa
20	$\text{LogH} = -3.9843 + 0.0024 \times C_w$	0.9865	1733
30	$\text{LogH} = -4.1166 + 0.0026 \times C_w$	0.9913	1651
40	$\text{LogH} = -4.0052 + 0.0026 \times C_w$	0.9932	1608
50	$\text{LogH} = -4.3210 + 0.0029 \times C_w$	0.9931	1551
20	$\text{LogH} = 1.7978 - 0.0167 \times C_e$	0.9927	
40	$\text{LogH} = 1.4948 - 0.0139 \times C_e$	0.9924	
60	$\text{LogH} = 1.9495 - 0.0177 \times C_e$	0.9969	

* H = the capacitance signal measured as peak height. C_w = the concentration of water vapour in the range from 1705 to 2197 Pa. C_e = the concentration of ethanol in water in the range from 20 % to 80 % (w/w) ethanol.

Table 3. Indirect measurements of ethanol present in drinks with the capacitance flow-through detector.

Sample number	Colour	Ethanol in present work / % (by wt)	Reference value* / % (by wt)
1	colourless	30.2 ± 1.8	32
2	yellowish-brown	33.5 ± 1.7	35
3	colourless	34.9 ± 1.5	36
4	colourless	41.0 ± 1.3	40
5	yellowish-brown	31.6 ± 1.9	34
6	light brown	36.2 ± 1.4	37
7	light yellow	36.6 ± 1.4	37
8	colourless	32.8 ± 1.6	35
9	colourless	37.4 ± 1.8	36
10	yellowish-brown	44.3 ± 1.5	42
11	colourless	33.8 ± 1.4	34
12	colourless	31.4 ± 1.4	31
13	colourless	35.0 ± 2.1	35
14	yellowish-brown	35.0 ± 1.3	35
15	violet	38.4 ± 1.4	38
16	brown	34.2 ± 2.2	35
17	light brown	35.8 ± 1.8	36
18	light yellow	38.6 ± 1.6	40
19	yellowish-brown	34.0 ± 1.6	35

*Reference values provided by the laboratory of drink analysis, at the Institute of Chemistry of São Carlos, University of São Paulo.

rectly determine ethanol in drinks. The capacitance detector can be used for "in line" measurement of ethanol content of drinks in beverage industries.

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