

## Study of the Naphthenic Corrosion of AISI 316 and AISI 1020 Steels by Light, Scanning Electron and Atomic Force Microscopies (LM, SEM and AFM)

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Corrosion processes were evaluated for AISI 316 and AISI 1020 steels by scanning electron microscopy (SEM), atomic force microscopy (AFM) and light microscopy. Coupons were immersed in four crude oil samples with different total acid numbers (TANs) for 48 days at room temperature. The steels were also exposed to three blends (B1-B3), produced by quaternary mixtures of the oils, with lower TANs than their respective original oils. SEM micrographs showed pitting-type corrosion in most cases. AFM imaging showed drastic changes in the peak-to-peak values, topographic profiles and phase images of the AISI 1020 coupons exposed to all oils and blend B3 as compared to the unexposed steel. Defects were produced on the surface of almost all the samples exposed to naphthenic corrosion. Exposure to the oil blends reduced the extent of the naphthenic corrosion on the coupons, especially blends B1 and B2. The oil mixtures (blends) reduced corrosion.

**Keywords:** corrosion, SEM, AFM, blends, AISI 316, AISI 1020

### Introduction

Naphthenic acids<sup>1</sup> (NAs) are carboxylic acids with the general formula  $R-(CH_2)_n-COOH$ , where R corresponds to one or more cyclopentane or cyclohexane rings.<sup>2</sup> Although NAs have been identified as major corrosive components in petroleum, this class of compounds represents only 3 wt.% of the organic composition of crude oils.<sup>3</sup>

Estimating the concentration of NAs in oils is a daily task in the petroleum industry and is measured by a potentiometric titration method that uses potassium hydroxide (KOH) solution. The result is the total acid number (TAN), defined as the amount of KOH (in mg) required to neutralize all acidic species in 1 g of petroleum, including NAs.<sup>4</sup>

Crude oils with TANs greater than 0.5 mg of KOH g<sup>-1</sup> may have more issues with corrosion.<sup>5,6</sup> Although this correlation is a commonly used gauge, in the literature,<sup>7</sup> TAN has been described as an unreliable indicator due to significant differences in the reported corrosiveness of oils with the same TAN. Apart from TAN and NA structure, other variables can also directly influence the corrosion caused by typical crude oil, such as salinity, total sulfur content, temperature, mechanical stress and microbiological action.<sup>8,9</sup>

The industry has been investing in more corrosion-resistant steels, such as AISI 316 stainless steel, as well as mixing heavy oils with light oils that have lower TANs (TAN < 0.5 mg KOH g<sup>-1</sup>),<sup>10</sup> to reduce the corrosive effects on distillation towers, ducts, and metal materials involved throughout the entire oil processing chain. The oil mixture is called a blend; it can be tailored to reduce viscosity,

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which improves its fluidity in all refining steps, and also to reduce TAN and total sulfur contents,<sup>11</sup> which are the primary causes of corrosion in oilseed plants.<sup>12</sup>

Several methods have been applied in the study of corrosion on metallic surfaces, such as electrochemical impedance spectroscopy (EIS), Raman and infrared (IR) spectroscopies, potentiostatic techniques, mass loss, light microscopy (LM) and scanning electron microscopy (SEM). Among these, LM and SEM have been widely used<sup>13-15</sup> because they allow structural, phase and morphological characterization of samples.<sup>16</sup>

Microscopic techniques such as SEM and atomic force microscopy (AFM) were employed by Marin *et al.*<sup>17</sup> to investigate the morphology of Al<sub>2</sub>O<sub>3</sub> and TiO<sub>2</sub> coatings on the surface of AISI 316 steel in order to improve intrinsic corrosion resistance. Dias *et al.*<sup>18</sup> also used SEM and AFM for monitoring naphthenic corrosion of AISI 1020 steel immersed in oils with different TANs (ca. 2.4 and 4.8 mg KOH g<sup>-1</sup>) and subjected to thermal treatments for different exposure times. The AFM results showed that the surface of the steel immersed in the higher TAN oil was severely altered.<sup>18</sup>

SEM can be coupled with energy dispersive spectroscopy (EDS), which provides qualitative and semi-quantitative elemental compositions for the surfaces of materials. Because the analyses are relatively fast and the sample preparation is easy, SEM is useful in the study of surfaces.<sup>19</sup> AFM is a high-resolution technique that provides *in situ* analyses of the surfaces of materials,<sup>15,20</sup> measuring topographical, structural and elastic properties. Moreover, AFM has superior performance when compared to other microscopic techniques such as LM and SEM.<sup>21,22</sup> AFM images have resolution in three dimensions, with magnifications on the order of millions,<sup>23</sup> making it possible to quantify the surface roughness of materials. In this work, we combined SEM and AFM

techniques to study the corrosion of AISI 316 and AISI 1020 steel caused by blends of oils and their respective crude oils.

## Experimental

### Preparation and characterization of oils and mixtures

Four crude oil samples were selected from a production field located in the sedimentary basin of the Brazilian coastal region: two offshore oils, designated P1 (American Petroleum Institute (API) 26.4, medium) and P2 (API 18.3, heavy); and two onshore oils, designated P3 (API 12.2, heavy) and P4 (API 19.6, heavy). These samples were analyzed in the Laboratory of Research and Development of Methodologies for Oil Analysis (LabPetro), Department of Chemistry (DQUI) at the Federal University of Espírito Santo (UFES).

Crude oil samples were collected in accordance with ASTM D5854.<sup>24</sup> The characterization process for the oils began with the removal of free water (water not emulsified in the oil). Next, the oils were subjected to gravitational decantation for 1 h.<sup>25</sup> The water content in the water-oil emulsions was measured.<sup>26</sup> Samples with a water content above 1% (v/v) were dehydrated by adding 200 µL of a commercial demulsifier at 60 °C and centrifuging at 1600 rpm for 15 min.<sup>27</sup> These oils were designated as “dehydrated oils”. After de-emulsification, the water content of the oils was measured again to verify that it was less than 1% (v/v). Physicochemical properties of the oils were then characterized, such as API grade,<sup>28</sup> density,<sup>29</sup> TAN,<sup>4</sup> kinematic viscosity,<sup>30</sup> and total sulfur.<sup>31</sup> The physicochemical characterization of the oils and mixtures is summarized in Table 1.

Using the four crude oils selected, 68 blends (Table S1, Supplementary Information (SI) section) were prepared as

**Table 1.** Physicochemical characterization of the oils and their respective mixtures

Physicochemical property	Oil				Blend		
	P1	P2	P3	P4	B1	B2	B3
API degree ± 1	26.4	18.3	12.2	19.6	22.5	30.0	20.4
Density at 20 °C / (g cm <sup>-3</sup> )	0.8916 ± 0.0002	0.9403 ± 0.0002	0.9801 ± 0.0002	0.9317 ± 0.0002	0.91890	0.91600	0.93130
TAN / (mg KOH g <sup>-1</sup> )	0.3645 ± 0.0013	2.3056 ± 0.0149	2.4150 ± 0.0320	1.3356 ± 0.0136	1.2156	1.0568	1.4620
Kinematic viscosity at 40 °C / (mm <sup>2</sup> s <sup>-1</sup> )	45.020 ± 0.026	365.74 ± 0.78	15567 ± 0	204.40 ± 0.27	119.53	113.905	259.645
Total sulfur / (% m/m)	0.15070 ± 0.0001	0.51901 ± 0.0002	0.49599 ± 0.00209	0.42028 ± 0.00040	0.34733	0.31797	0.36856

P: crude oil; B: blends; API: American Petroleum Institute; TAN: total acid number.

**Table 2.** Concentrations of the oils P1, P2, P3 and P4 used for the production of three blends

Blend	Oil P1 / wt. %	Oil P2 / wt. %	Oil P3 / wt. %	Oil P4 / wt. %
B1	39.77	20.68	9.50	30.05
B2	49.93	10.63	10.05	29.39
B3	39.62	10.80	30.08	19.50

planned over five levels (with 5<sup>4</sup> possible combinations) with Minitab<sup>32</sup> 14.0 software. For the corrosion tests and analyses by SEM and AFM, only three blends were selected (B1, B2, and B3, Table 2), considering the greater impact of crude oil P1, which had the lowest TAN, and thus acted as a diluent.<sup>33</sup> SEM and AFM analyses were performed after the samples were immersed in the dehydrated oils and in the selected blends to identify possible corrosion processes in AISI 316 stainless and AISI 1020 carbon steels.

#### Corrosion assays

Samples of AISI 316 and AISI 1020 steel with a 7.83 cm<sup>2</sup> area were washed with acetone, polished with 120- to 1220-grit sandpaper and immersed in an ultrasonic bath for 10 min with P.A. (proanalysis grade) acetone for 20 min.<sup>18</sup> The coupons were dried with an air drier and immersed in 10 mL of the oils and their respective blends in closed containers. The steel samples were exposed to the oils and blends for a total of 48 days at room temperature (23 °C) and 1 atm pressure, and the conditions were static. The coupons were then removed from the oils and blends, washed with kerosene and acetone, and dried. The surface of each steel was subsequently analyzed by LM, SEM, and AFM.

#### LM, SEM, and AFM analyses

Triplicate SEM micrographs were collected at 1000 and 5000 times magnification using a Zeiss EVO 50 scanning electron microscope (Jena, Germany) operated at 12 kV, without metallization of the samples. The AFM images were collected using an alpha300 R confocal microscope (WITEc, Wissenschaftliche Instrument und Technologie GmbH, Ulm, Germany) operated in non-contact mode (from regions selected using a light microscope, LM), with a Si<sub>3</sub>N<sub>4</sub> cantilever, a nominal constant of 42 N m<sup>-1</sup>, a resonant frequency of approximately 285 kHz, scan rates of 0.3-1.0 Hz, and scan sizes of 2,500-10,000 nm.<sup>17</sup> In addition to topographic images, phase and LM images were collected simultaneously. Phase images were used to estimate the physical properties of the AISI 316 steel, such as hardness, adhesion, and viscoelasticity.<sup>34,35</sup>

Surface asymmetry (Ssk), obtained from equation 1, and peak-to-peak height, given by the difference between the highest and lowest peak heights, were used to assess surface roughness. Surface asymmetry was calculated as follows:

$$Ssk = \frac{1}{R_Q^3} \frac{1}{n} \sum_i^n Z_i^3 = Z_i^3 \quad (1)$$

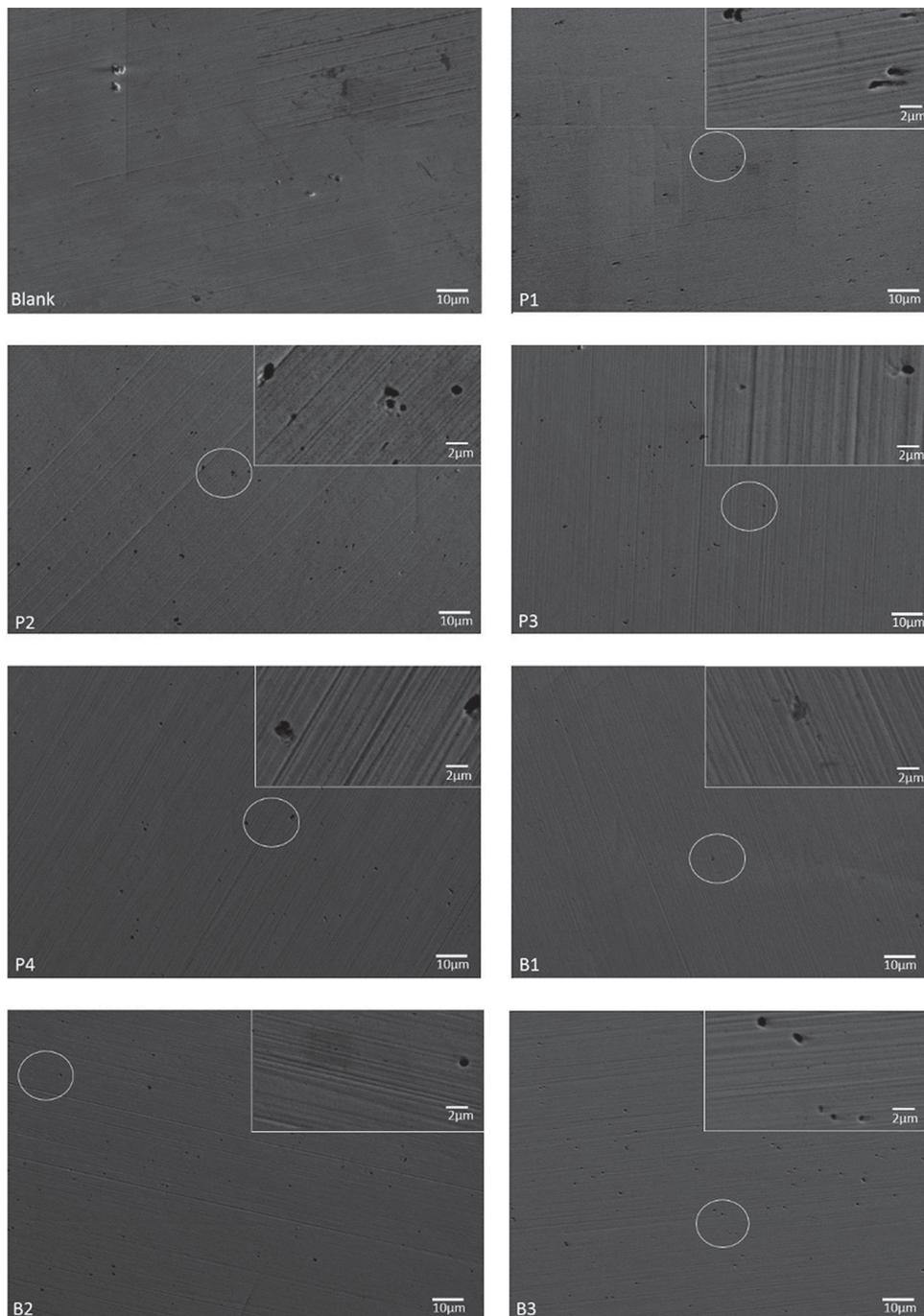
where  $Z_i$  is the height at position  $i$ ,  $R_Q$  is the quadratic mean of the height deviation, and  $n$  is the number of points within the image grid. In general, an Ssk of zero suggests a symmetric data distribution or an even data distribution around the mean plane, while a non-zero Ssk suggests an asymmetric distribution, where a flat surface with small peaks (Ssk > 0) or small valleys (Ssk < 0) is observed.<sup>36</sup>

## Results and Discussion

#### SEM analysis

Figure 1 shows SEM images of the AISI 316 steel coupons before and after exposure to crude oils (P1, P2, P3, and P4) and their respective blends (B1, B2, and B3); the images provided morphological details of the steel surfaces. A resolution of 2 μm was achieved, with magnifications of 1000 × and 5000 ×, which identified that all the oils altered the surfaces of the steels compared to the unexposed samples. Pitting observed on the surfaces of the oil-exposed AISI 316 steel coupons was indicative of corrosion. Pitting-type corrosion occurs when the depth of the eroded area is greater than the diameter of the same area.<sup>37</sup> The defects formed on the surfaces of the AISI 316 steels, shown in Figure 1, presented similar degrees of corrosion from all the oils studied.

With the aim of better evaluating and distinguishing the effects of naphthenic corrosion caused by different crude oils, the AISI 1020 carbon steel, which has lower corrosion resistance, was also submitted to assays, and the results are shown in Figure 2. The corrosion process was quite different among the crude oil samples, with more severe corrosion seen on the coupons immersed in crude oils P2 and P3, whereas crude oils P1 and P4 caused less corrosion. Corrosion affected the samples in the following order of impact: P4 ≈ P3 > P2 > P1



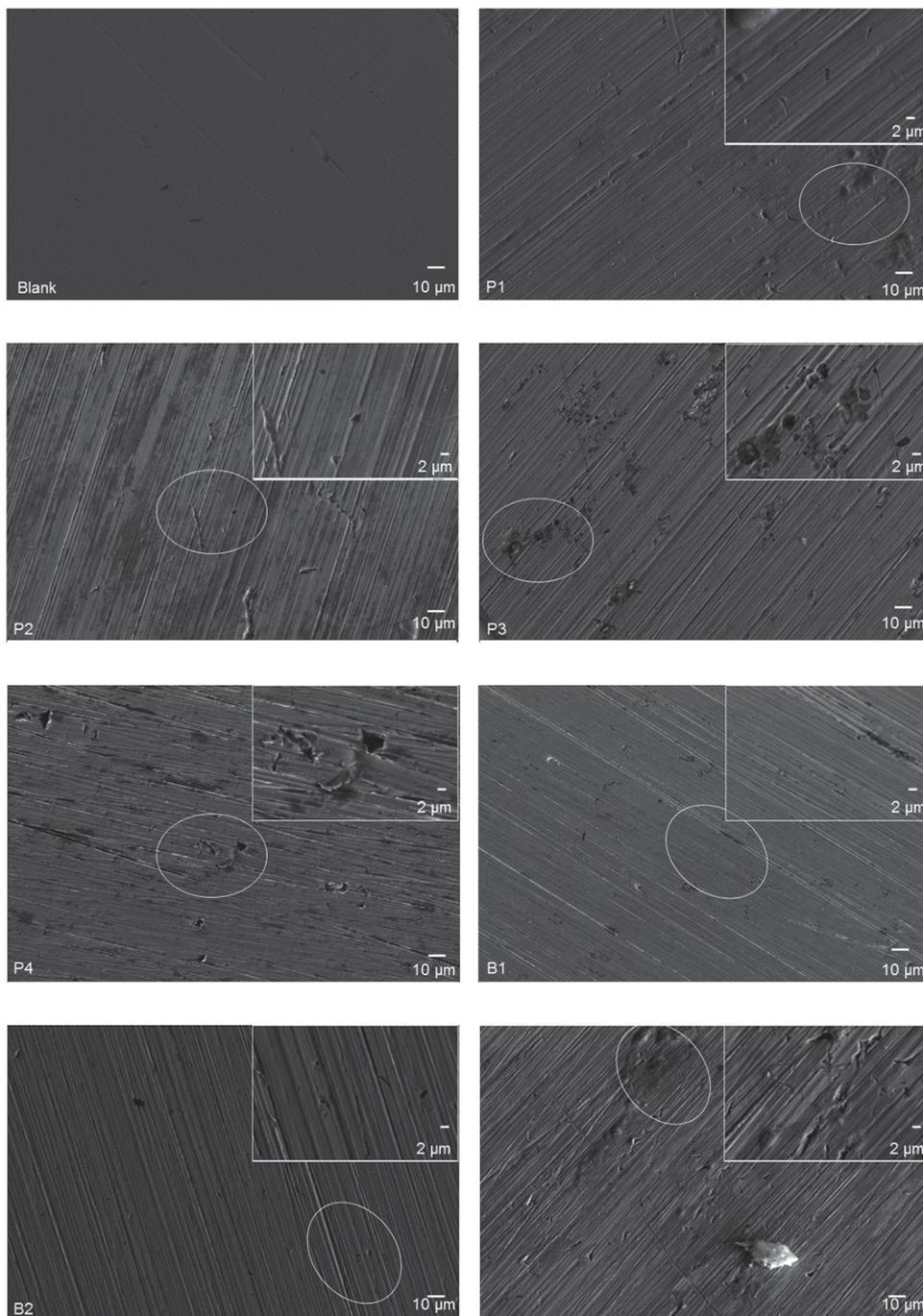
**Figure 1.** SEM images of the AISI 316 steel coupons before (blank) and after exposure to the crude oils (P1, P2, P3, and P4) and their blends (B1, B2, and B3). For each image, a 5000 × amplification was made to the circled regions. The coupon nomenclature refers to the oil in which it was immersed.

(Figure 2). This corrosive behavior was expected, since oils P3 and P4 have comparatively high TANs and total sulfur content (P3: TAN =  $2.4150 \pm 0.0320$  mg KOH g<sup>-1</sup> and total S =  $0.49599 \pm 0.00209$  wt.%; and P4: TAN =  $1.3356 \pm 0.0136$  mg KOH g<sup>-1</sup> and total S =  $0.42028 \pm 0.00040$  wt.%, Table 1).

The number of defects produced in both steels (Figures 1 and 2) from exposure to the blends was drastically lower than that produced from exposure to the crude oils. For

the blends, corrosion affected the samples in the following order of impact: B3 > B2 > B1. When comparing the corrosive behavior among the two subsets of data (blends B1-B3 and oils P1-P4), the blends had, in most cases, lower TANs ( $1.0568$ - $1.4620$  mg KOH g<sup>-1</sup>) and total sulfur content ( $0.31797$ - $0.36856$  wt.%), as shown in Table 1, proving that the blending process was efficient at reducing corrosion.

Although many studies in the literature, such as those by Huang *et al.*<sup>38</sup> and Dalmaschio *et al.*,<sup>39</sup> report a correlation



**Figure 2.** SEM images of the AISI 1020 steel coupons before (blank) and after exposure to the crude oils (P1, P2, P3, and P4) and their blends (B1, B2, and B3). For each image, a 5000 × amplification was made to the circled regions. The coupon nomenclature refers to the oil in which it was immersed.

between the physicochemical characteristics of petroleum and corrosion, Jayaraman *et al.*<sup>40</sup> consider TAN to be a very superficial estimate for corrosion. For example, we can look at the corrosion behavior observed after exposure to oil P2. Oil P2 had the highest TAN and total S content among all the oils analyzed (TAN =  $2.3056 \pm 0.0013$  and total S =  $0.51901 \pm 0.0002$  wt.%, Table 1). However, its degree of corrosivity was similar to oil P1, as shown in Figure 2. Therefore, this behavior was due to the structure and

functionality of the NAs, which can directly interfere with corrosion.<sup>41</sup> Deyab *et al.*<sup>42</sup> have proved that the molecular weight of NAs influences naphthenic corrosion. Naphthenic corrosion may also be influenced by other factors, such as the salt content and sulfur compounds, as well as the concentration of naphthenates.<sup>42,43</sup>

Regarding the blends, the exposure of AISI 316 steel to blend B1 (Figure 1) also changed its surface. Although the corrosive impacts of blend B1 were low (Table 1), it was

the only oil that presented alveolar-type corrosion, which is characterized by eroded areas with greater diameter than depth.<sup>44</sup> Alveolar and pitting corrosion are types of corrosion that result from damage to the uniformity of the passive film, such as rupture, which quickly exposes the surface to attack and leads to localized corrosion.<sup>45,46</sup> Similar corrosive attacks were seen by Freitas *et al.*,<sup>47</sup> who also found these two types of corrosion in samples of AISI 1020 steel exposed to crude oil and their respective distilled cuts.

The results observed and discussed here demonstrated the challenge and complexity of the study of corrosion in petroleum and petrochemical plants. Therefore, despite many research studies in this area since the discovery of naphthenic corrosion in 1920,<sup>3</sup> its occurrence has not yet been fully elucidated.

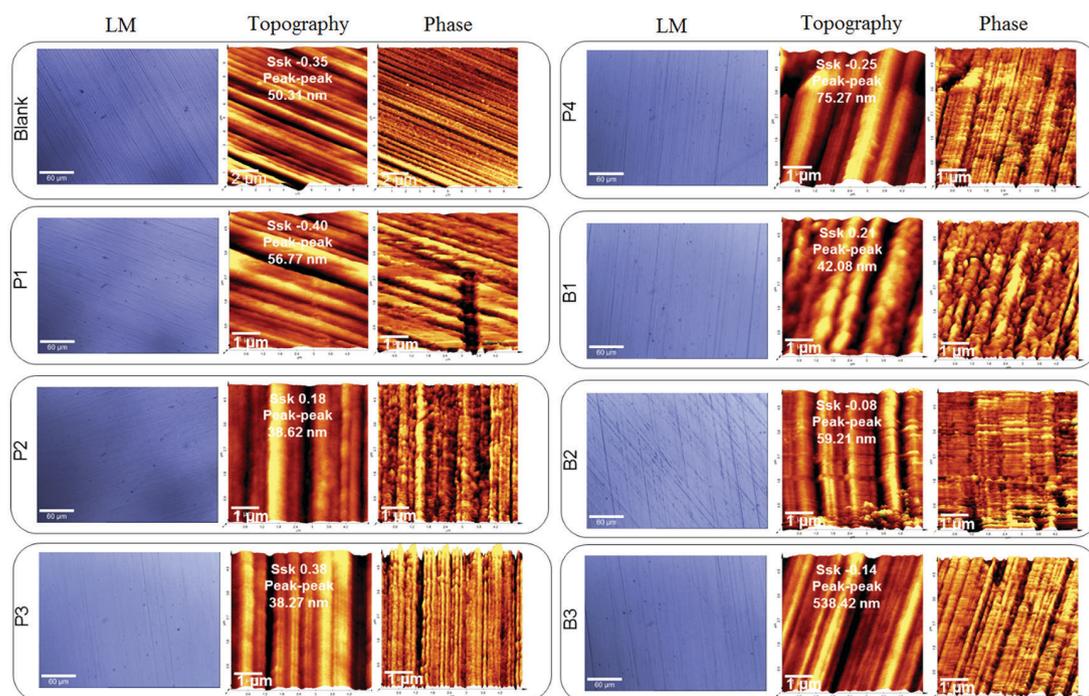
#### LM and AFM analysis

Figure 3 shows the LM images and AFM phase and topography images of the surface of the AISI 316 steel samples before (blank) and after exposure to different crude oils (P1-P4) and their respective blends (B1-B3) for 48 days. The LM images (Figure 3) appeared to be the same for all oils and blends tested. Although LM is widely applied in corrosion analysis,<sup>48-50</sup> its scale often makes it difficult to see the initial phases of corrosion. The relatively noble nature of the stainless steel chosen for this study (AISI 316) also contributed to this phenomenon.<sup>17</sup>

Topography images of AFM for the surface of the steel (blank) showed evidence of a continuous and standardized structure, as seen in Figure 3.<sup>51</sup> The most prominent features in the LM images were scratches produced by the polishing process, which do not cause any changes in the nanostructure but only alter the average surface ripple,<sup>52</sup> which was measured as a peak-to-peak height of 51 nm. The data are shown in Table 3. These values were greater than or similar to that for the unexposed blank for the samples exposed to the less corrosive oils and blends, such as P1 and B2 (P1 = 57 nm and B2 = 59 nm). Conversely, the topographic and phase profiles were remarkably altered on the samples exposed to the more corrosive oils, such as P2-P4, as shown in Figure 3.

Changes were observed in the phase images of the AISI 316 steel samples exposed to oil P1 and blend B1 that were not observed in the LM, SEM and topographic images (Figures 1 and 3). The phase images show both physical changes and those of an elastic nature.<sup>34</sup> These images can be used to gauge changes in the surface of the material; thus, in this study, they were used to gauge the corrosion intensity.<sup>53</sup>

Tozzi *et al.*<sup>33</sup> studied the physicochemical properties of the original oils and their respective blends ( $n = 68$ ), noting that the kinematic viscosity, API grade, TAN and total sulfur can be reduced or improved when certain blends are produced. Similarly, the blends studied here (B1 and B2) caused less corrosion than their respective original oils,



**Figure 3.** LM images and AFM 3D topography and phase images for the AISI 316 steel surface before (blank) and after their immersion in different crude oils (P1-P4) and their respective blends (B1-B3). The coupon nomenclature refers to the oil in which it was immersed.

**Table 3.** Roughness data for the steel samples

	Treatments performed	AISI 316		AISI 1020	
		Ssk	Peak-to-peak height / nm	Ssk	Peak-to-peak height / nm
Crude oil	blank	-0.35	50.61	-1.07	104.35
	P1	-0.40	56.77	0.30	345.18
	P2	0.18	38.62	-0.52	576.06
	P3	-0.38	38.37	-0.15	296.82
	P4	-0.25	75.27	-0.20	415.42
Blend	B1	0.21	42.08	-0.18	290.90
	B2	-0.08	59.21	-0.19	282.18
	B3	-0.13	38.42	0.22	286.55

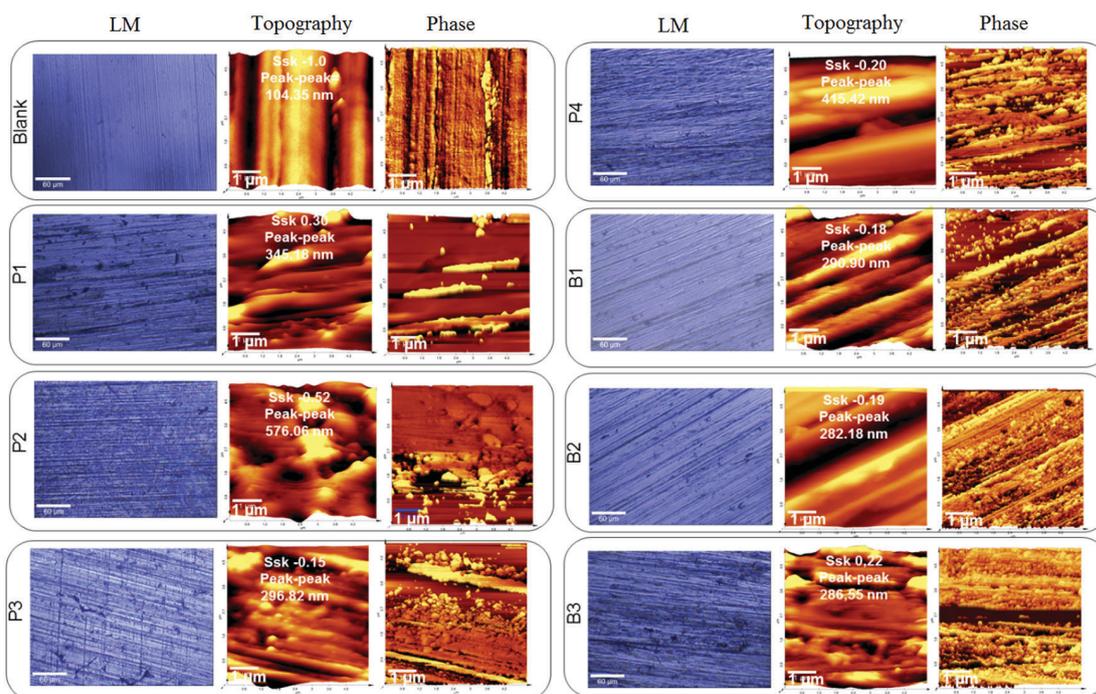
Ssk: surface asymmetry values.

even presenting changes in the phase images. Despite some corrosion under exposure to the blends, the AISI 316 steels exposed to blends B1 and B2 showed higher resistance to the corrosive attacks of NAs. Therefore, these mixtures reduced the effects of the corrosive processes.

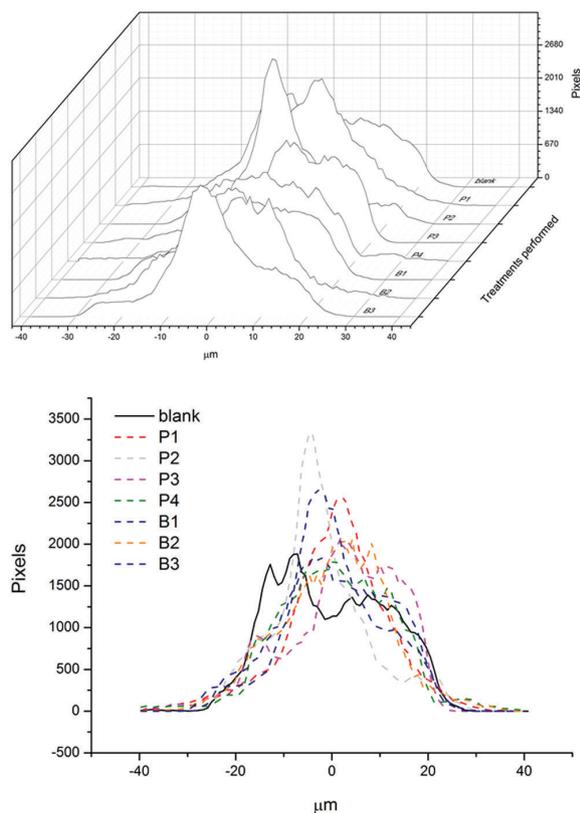
Figure 4 displays the LM images and AFM 3D topography and phase images for the AISI 1020 steel coupons surface before (blank) and after immersion in crude oils (P1-P4) and their respective blends (B1-B3). In the LM images, naphthenic corrosion was seen on AISI 1020 steel in all cases and was more severe for the oils P1-P4 and blend B3. As a consequence, the topographic and phase images were drastically different, with higher

peak-to-peak heights measured primarily for the crude oil exposures (P1-P4 = 297-576 nm and blank = 104 nm), as seen in Table 3.

The topographic behavior obtained by the AFM analysis shown in Figures 3 and 4 was better visualized by the histograms shown in Figures 5 and S1 (SI section). The AISI 316 steel coupons exposed to oils P3 and P4 and blends B1 and B2, as shown in Figure 5, presented topographic profiles that were very similar to that of the original sample, i.e., without the presence of a high peak and with a distributed area of  $-30$  to  $30$   $\mu\text{m}$ . Conversely, the surface of the sample exposed to P2 was altered the most severely of all samples tested, followed by the



**Figure 4.** LM images and AFM 3D topography and phase images for the AISI 1020 steel surface before (blank) and after their immersion in different crude oils (P1-P4) and their respective blends (B1-B3).



**Figure 5.** Histograms of the topography images obtained by AFM for AISI 316 steel before (blank) and after exposure to different crude oils and their respective blends.

sample exposed to blend B3. Consequently, a large and well-defined peak containing approximately 2000 pixels was seen.

Roughness data analysis is important in the study of the texture of a material and concerning the surface performance.<sup>54</sup> The roughness data (Table 3), expressed by the parameter Ssk, suggest the symmetry or lack thereof of a sample surface. For the original coupons (blank), which had Ssk of  $-0.35$  and  $-1.07$  (Figures 3 and 4, respectively), an asymmetrical surface was observed with a predominance of valleys. Conversely, the AISI 316 coupon exposed to oil P2 experienced a change in Ssk to 0.18, indicating the formation and predominance of peaks and an inversion in the height distribution on the steel surface. Similar behavior occurred on the coupon exposed to blend B1, with a change in Ssk to 0.21. However, the other coupons showed subtle changes in roughness.

Rios *et al.*<sup>54</sup> characterized the initial phase of corrosion of API 5L X70 steel in mineral oil that contained NAs as a function of time at room temperature, using electrochemical and microscopy techniques such as LM and AFM. The authors obtained micrographs of the metal surfaces at different immersion intervals ( $t = 6, 12, 24, 60$  and  $90$  min). Corrosion products formed rapidly, as observed after

12 min of exposure, progressively increasing up to 24 min.<sup>54</sup> Therefore, as in this work, the authors saw naphthenic corrosion at temperatures much lower than those typically studied in corrosion tests ( $T > 200$  °C).<sup>18,38,47</sup>

## Conclusions

In this work, two powerful microscopy techniques, SEM and AFM, were used to study the microstructure of the surfaces of corroded steels. SEM provided characterization of the type of naphthenic corrosion seen on the surfaces of the AISI 316 and AISI 1020 steels. AFM provided *in situ* analysis of the actual corrosion progression of the samples, even in the initial stages, through topography and phase images.

Naphthenic corrosion was seen on samples exposed to light and heavy oils containing a wide range of TANs ( $0.36$  to  $2.41$  mg KOH  $g^{-1}$ ). However, although some corrosion was also caused by the blends, blend B1 differed from the other oils, causing little erosion on the steel surface. The blends produced were also able to reduce the extent of corrosion compared to the original oils.

## Supplementary Information

Supplementary data are available free of charge at <http://jbcbs.sbj.org.br> as PDF file.

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